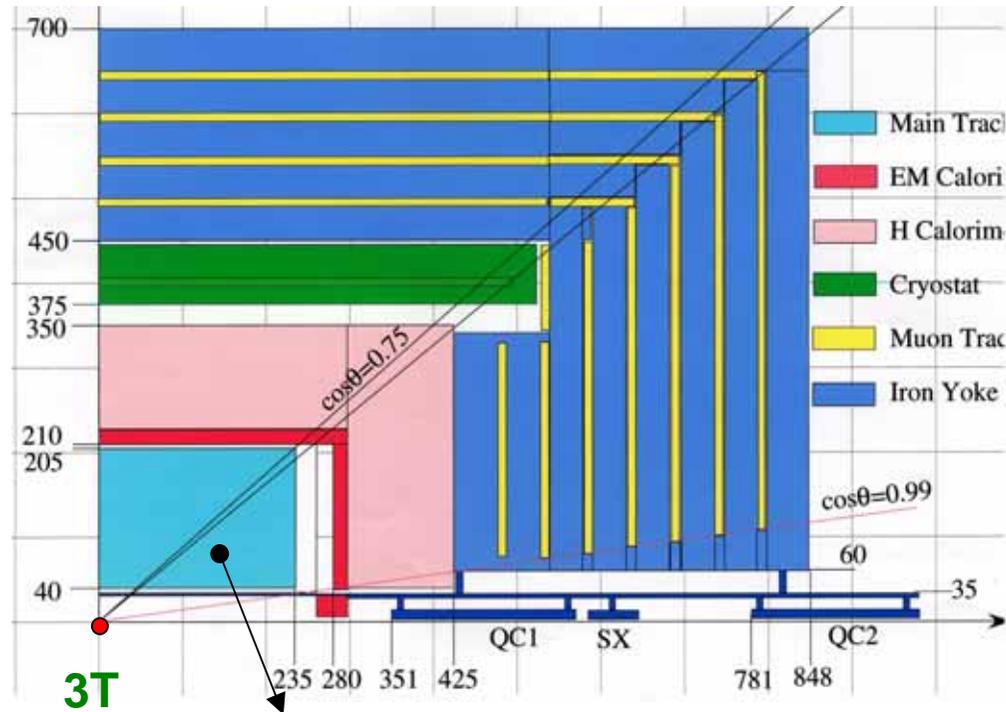


Support and magnet coil

KEK Hiroshi Yamaoka

Initial configuration of the iron yoke



$$\int_0^{z_{\max}} \frac{Br}{Bz} dz < 2mm$$

→ $\int_0^{z_{\max}} \frac{Br}{Bz} dz = 2.3 - 8mm$

Too large!!

→ Further amount of iron is necessary.

→ Iron Yoke configuration is optimized!

Material for return yoke

S10C(JIS)

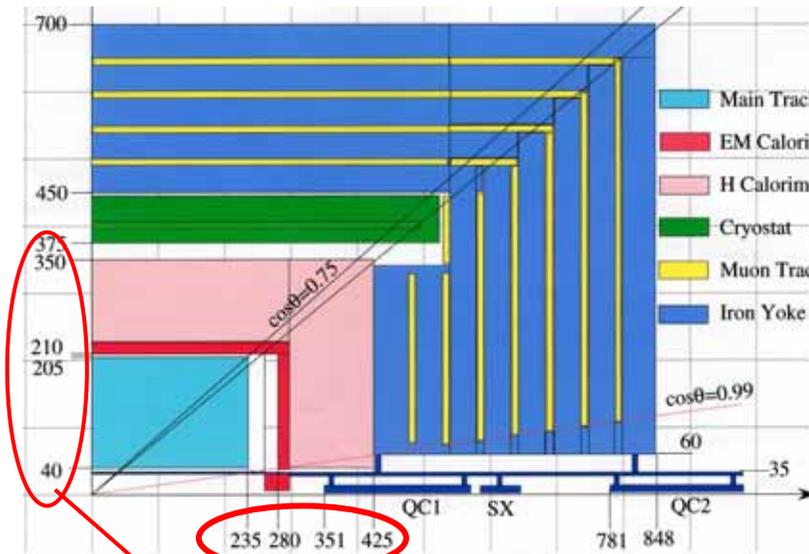
Carbon= 0.1wt%

$\sigma_t=310\text{MPa}$

$\sigma_e=205\text{MPa}$

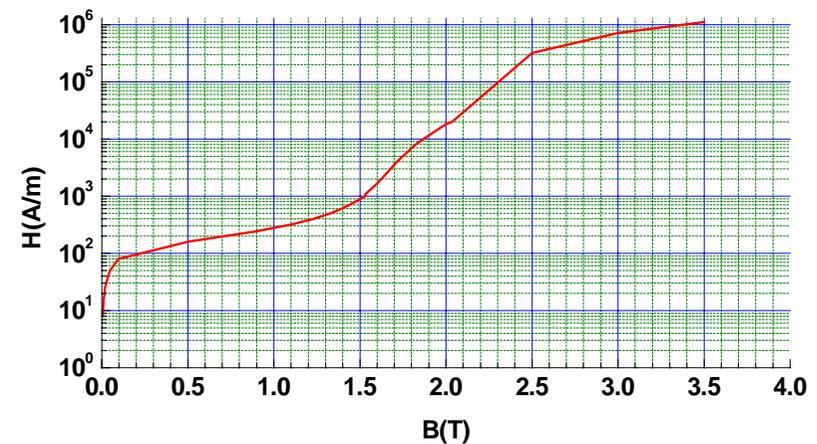
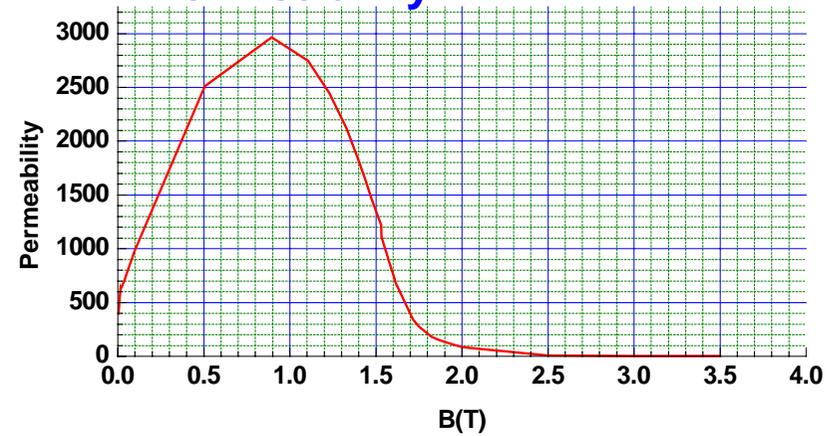
$\sigma_{\text{allow}}=120\text{MPa}$

Belle

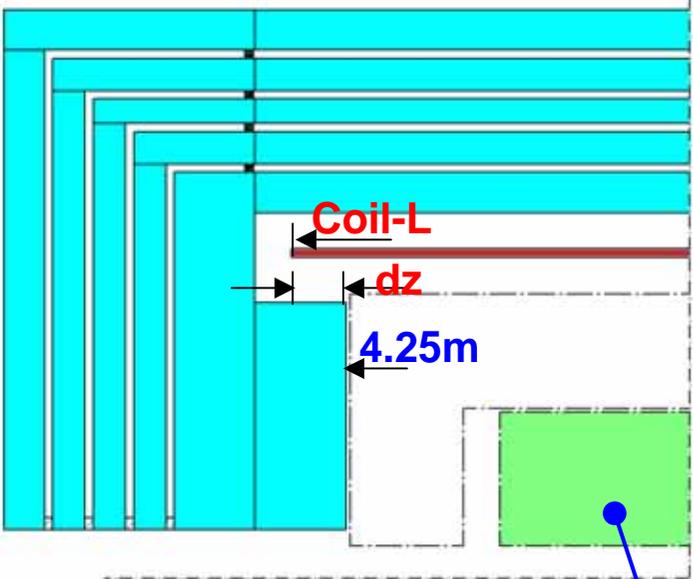


These dimensions are fixed,
Coil length, yoke dimensions are changed.

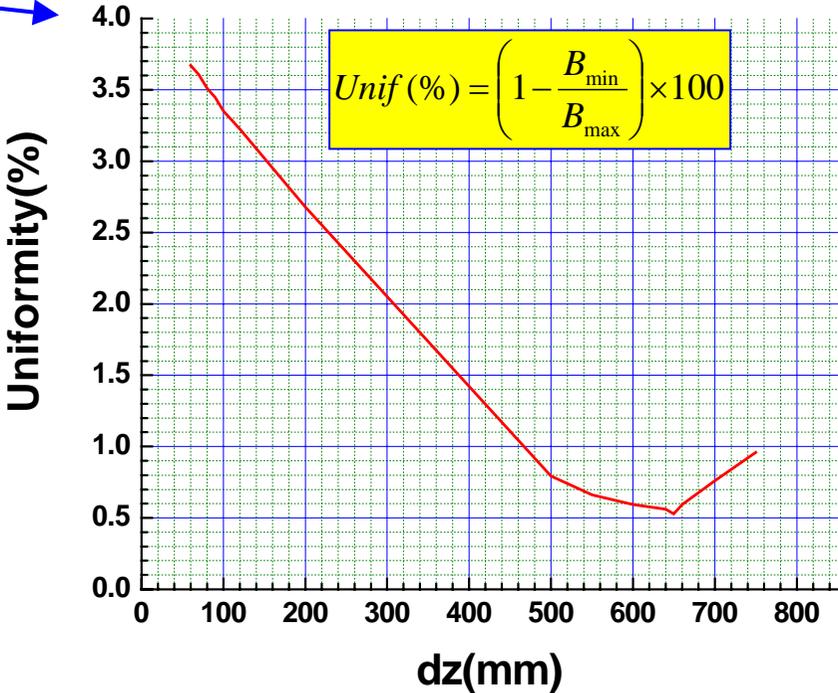
Permeability

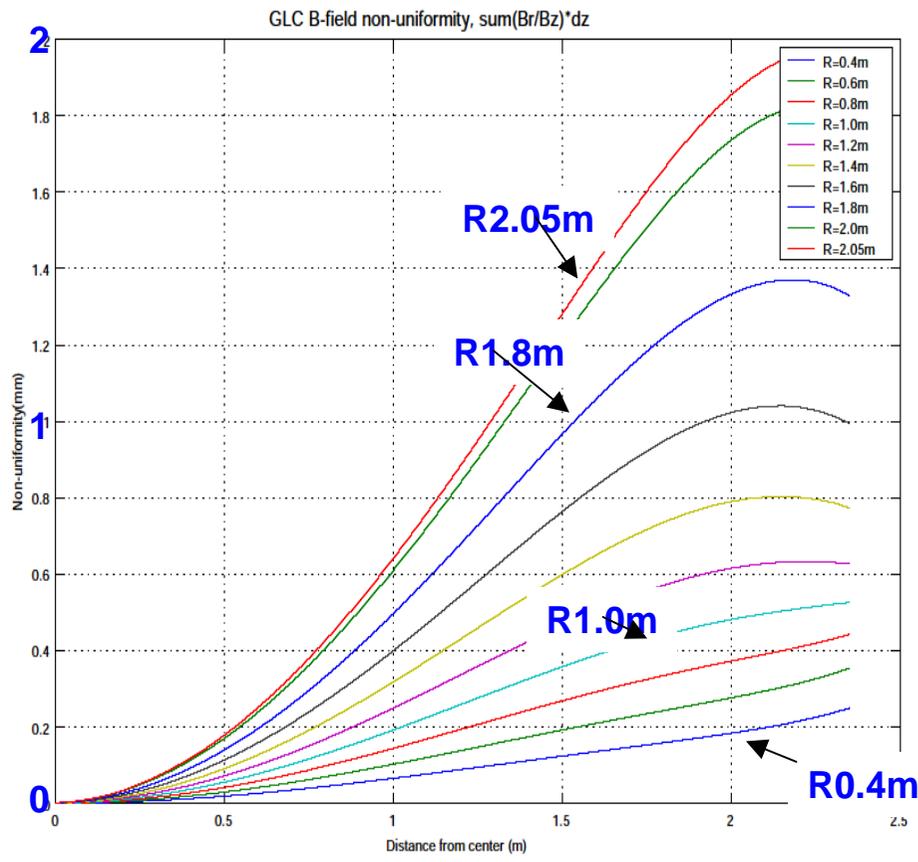
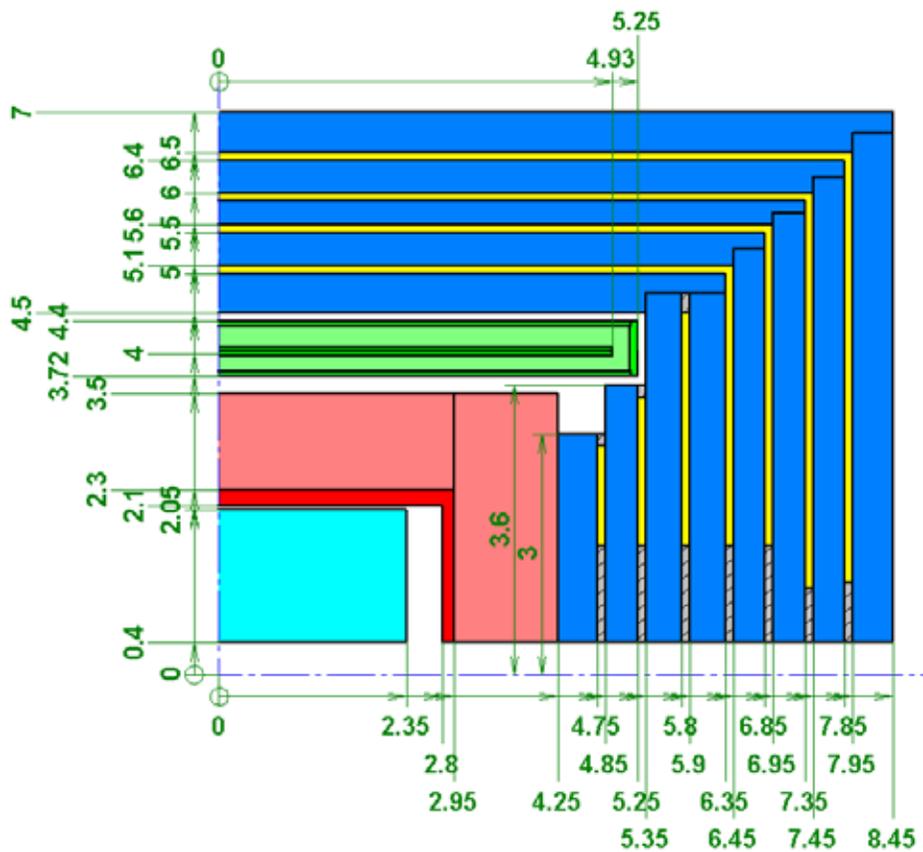


Calculations

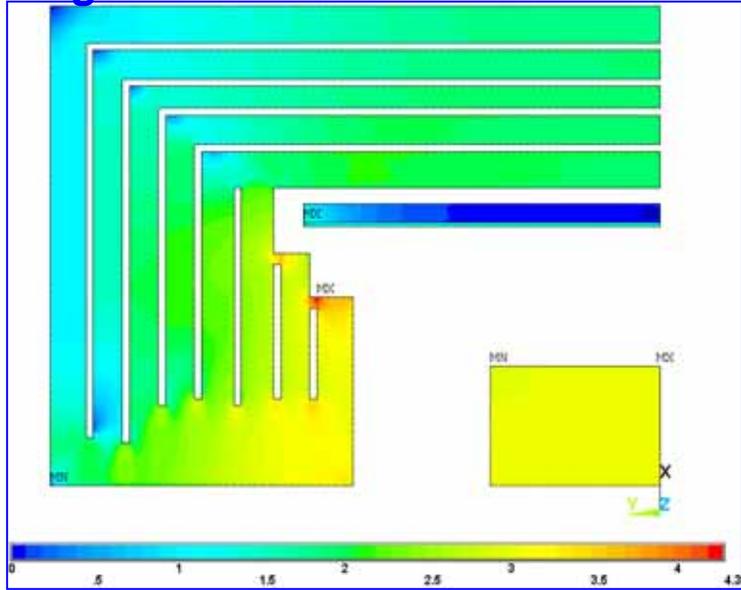


dz	Coil-L	Bmin	Bmax	Bc	Unif(%)
60	4.31	2.965	3.078	3.05	3.671
70	4.32	2.966	3.077	3.049	3.607
80	4.33	2.968	3.076	3.049	3.511
90	4.34	2.968	3.074	3.048	3.448
100	4.35	2.97	3.073	3.047	3.352
120	4.37	2.972	3.071	3.046	3.224
200	4.45	2.979	3.061	3.042	2.679
500	4.75	3.003	3.027	3.023	0.793
550	4.8	3.005	3.025	3.017	0.661
600	4.85	3.008	3.026	3.017	0.595
640	4.89	3.01	3.027	3.014	0.562
650	4.9	3.01	3.026	3.013	0.529
660	4.91	3.009	3.027	3.013	0.595
700	4.95	3.004	3.027	3.01	0.76
750	5	2.999	3.028	3.006	0.958

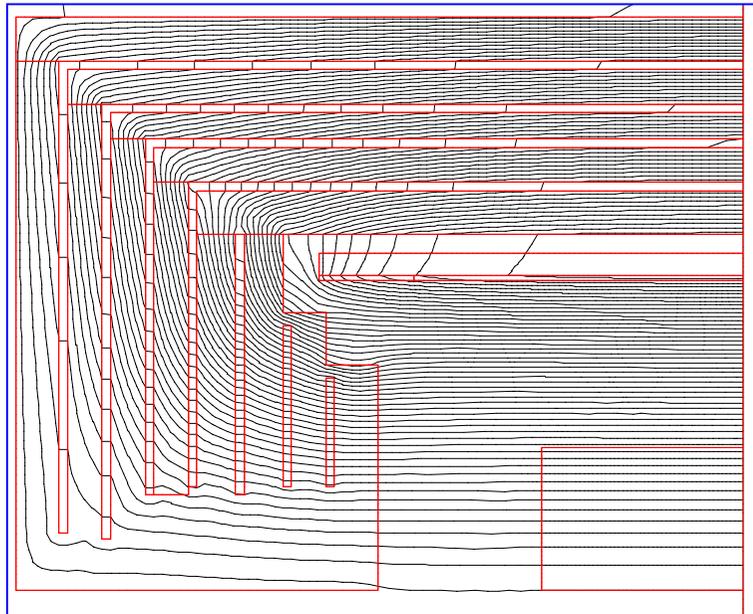




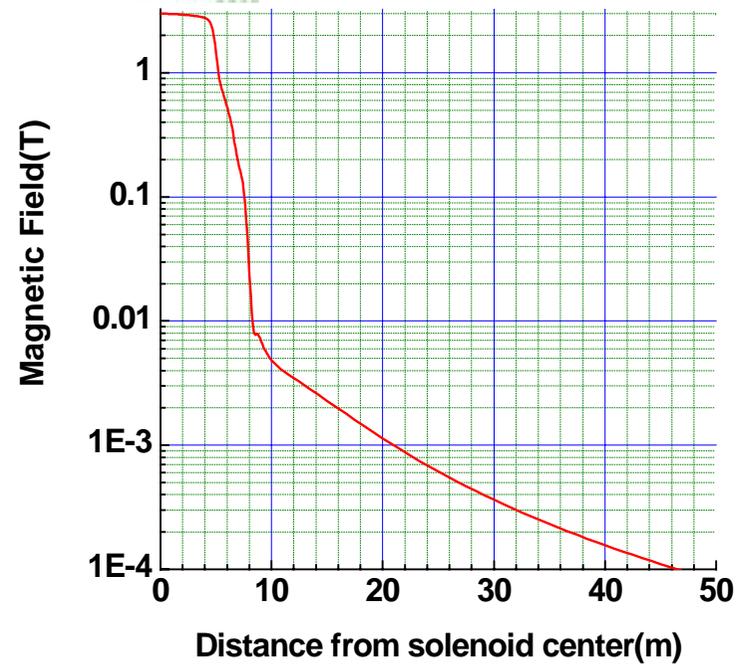
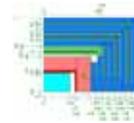
Magnetic field distribution



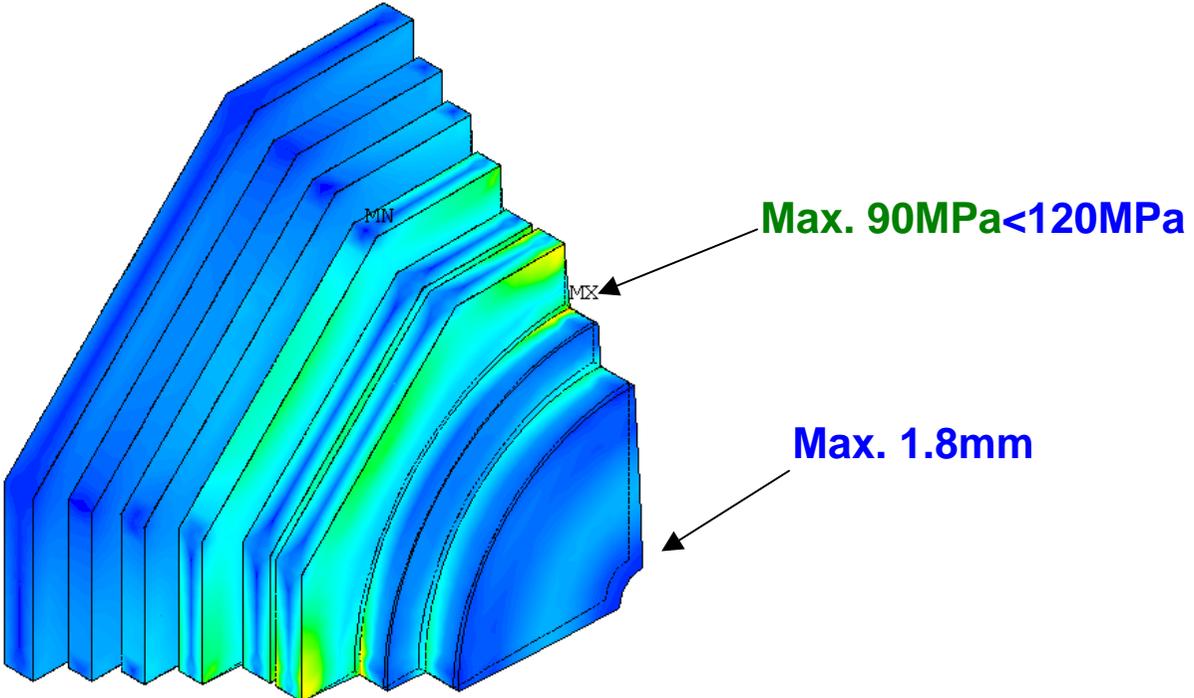
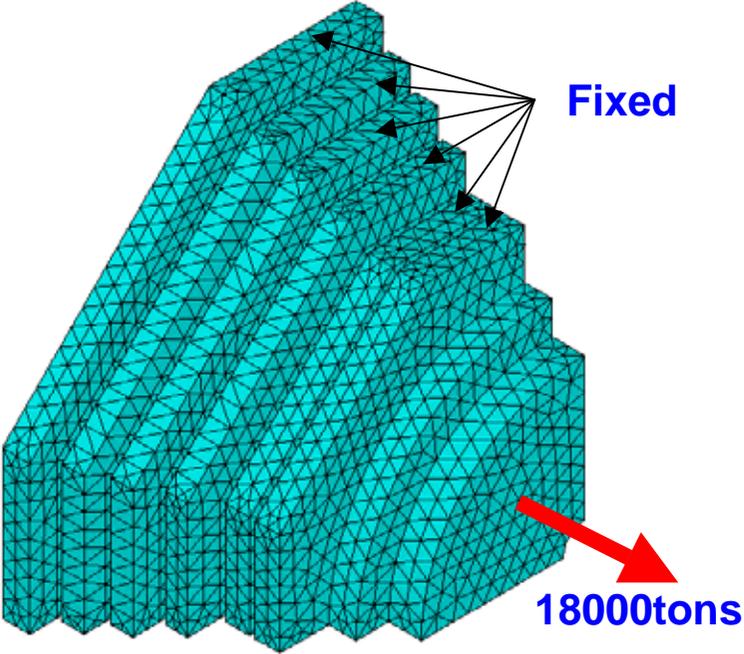
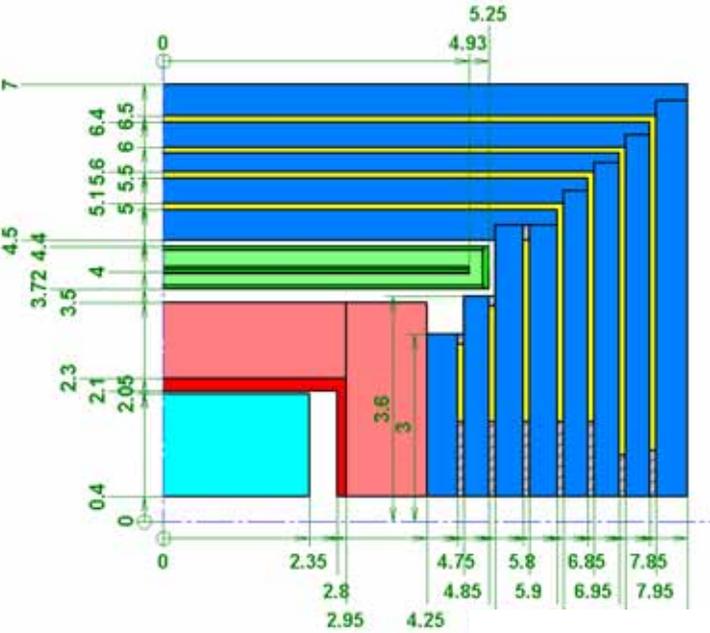
Flux line



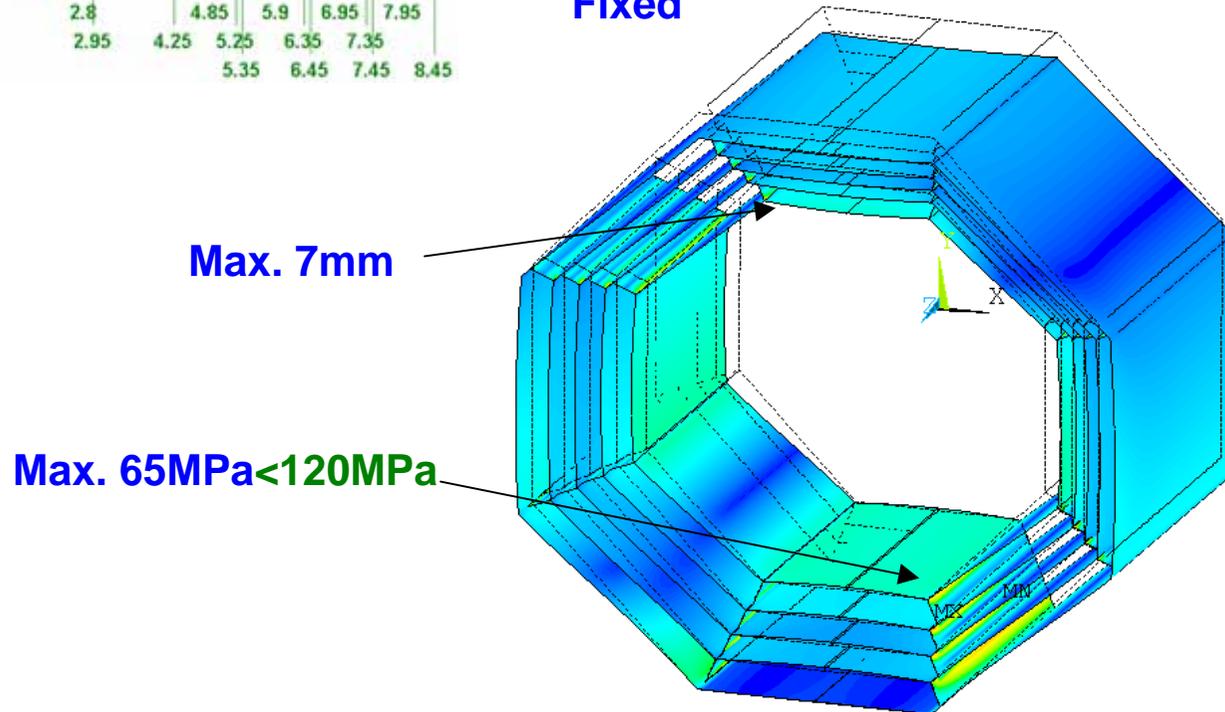
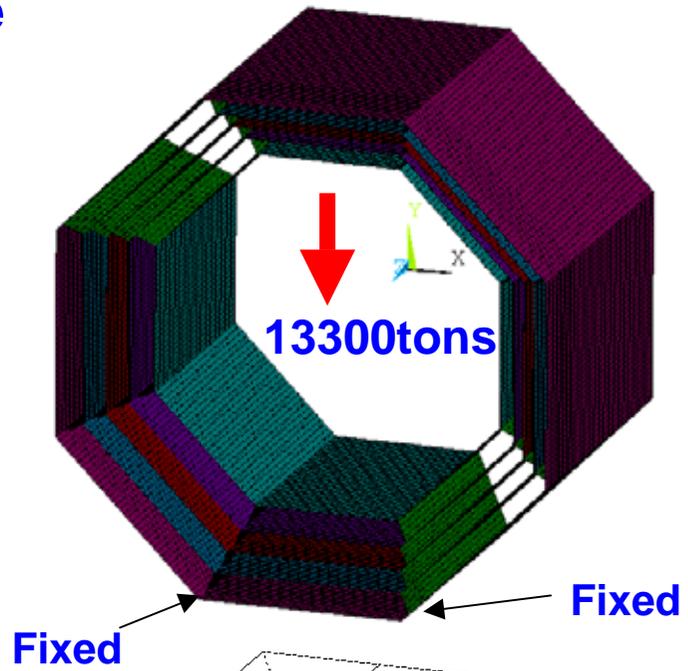
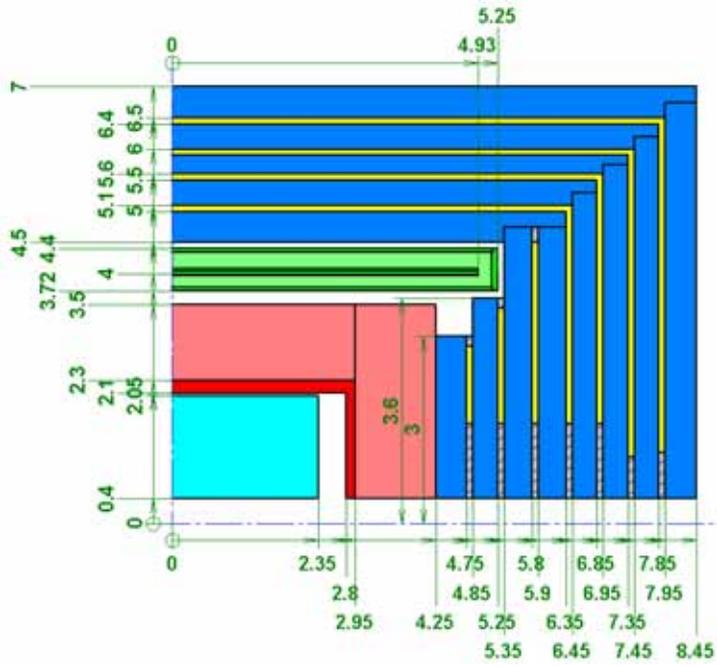
Fringe/Leakage field



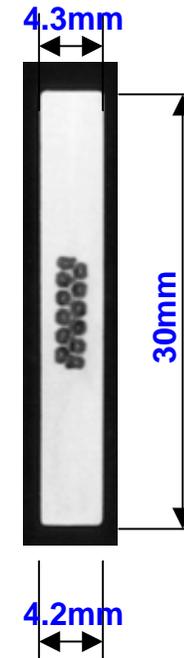
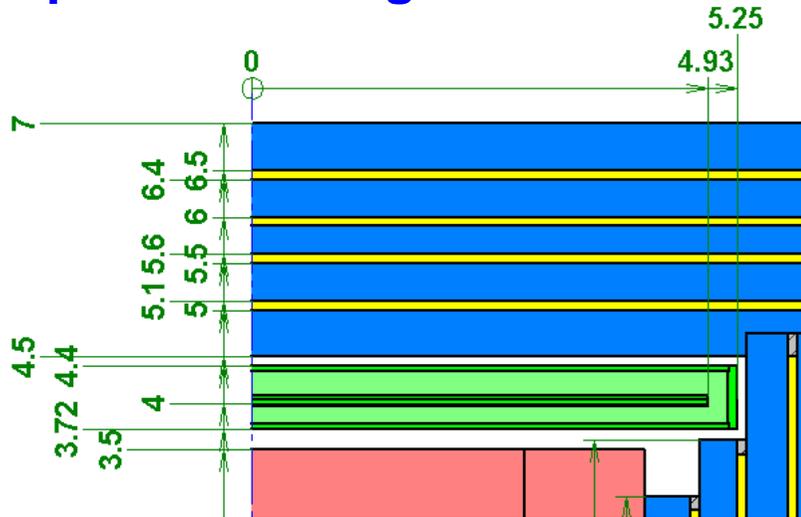
Stress/deformation of End Yoke



Stress/deformation of Barrel Yoke



Superconducting Solenoid



(For ATLAS)

Cryostat	Inner radius	3.72m
	Outer radius	4.4m
	Half length	5.25m
Coil	Mean radius	4.0m
	Half length	4.93m
Central magnetic field		3T
# of turns(2 layers)		4576 turns
Current density		741A/mm²
Nominal current		5338A
Inductance		81.0H
Stored Energy		1.8GJ

Aluminum stabilized superconductor

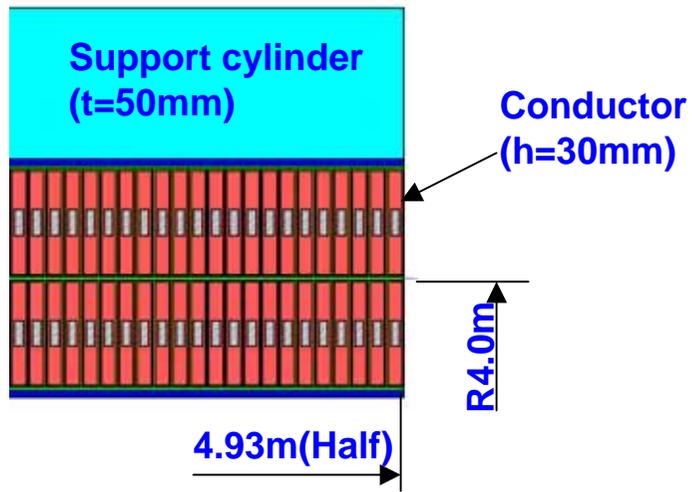
NbTi:Cu:Al= 1:0.9:15.6

Strand diameter: 1.23mm

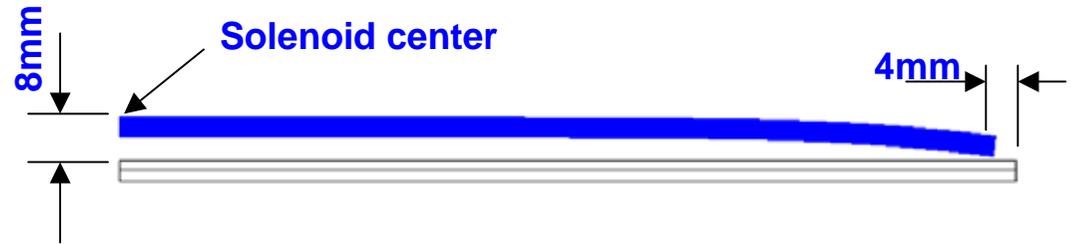
Filament diameter: 20μm

Jc in NbTi at 5T, 4.2K: > 2750A/mm²

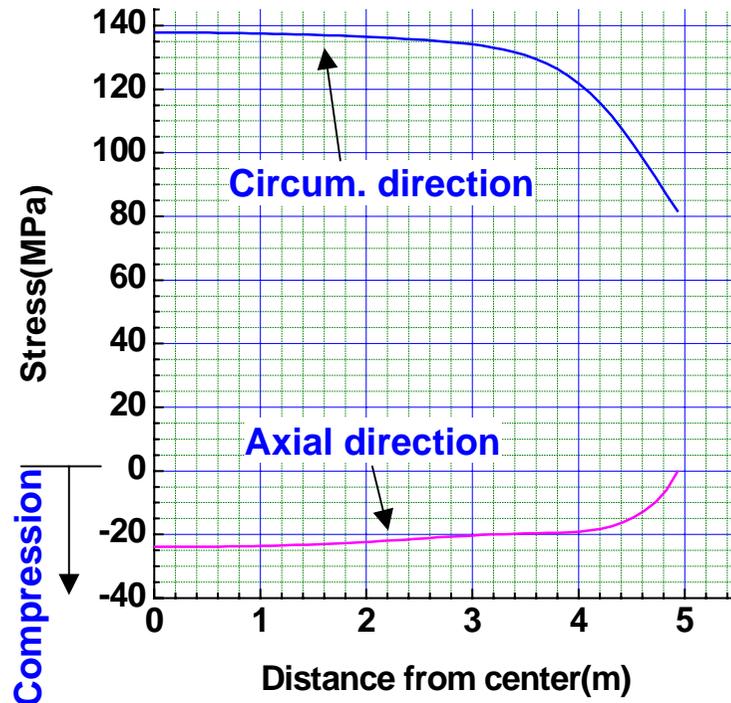
Ic at 5T, 4.2K: > 20300A



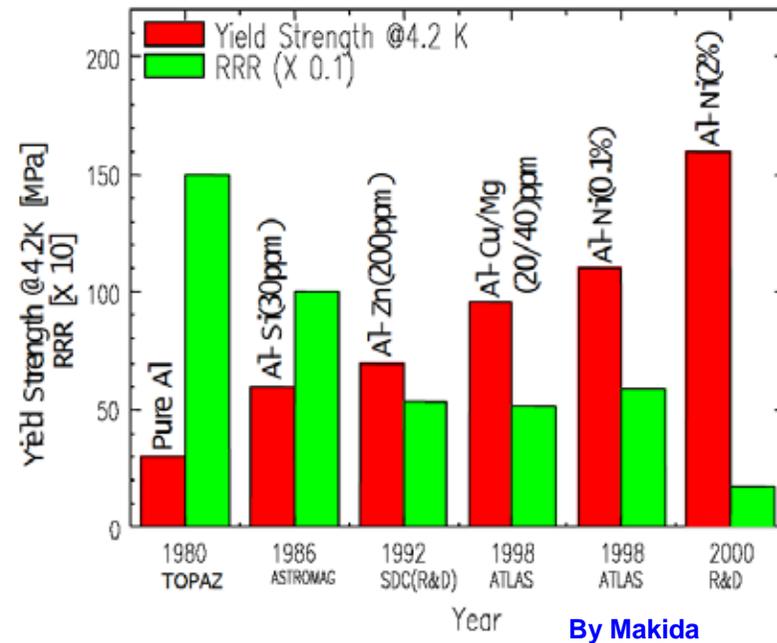
Deformation of the coil



Stress level in the coil

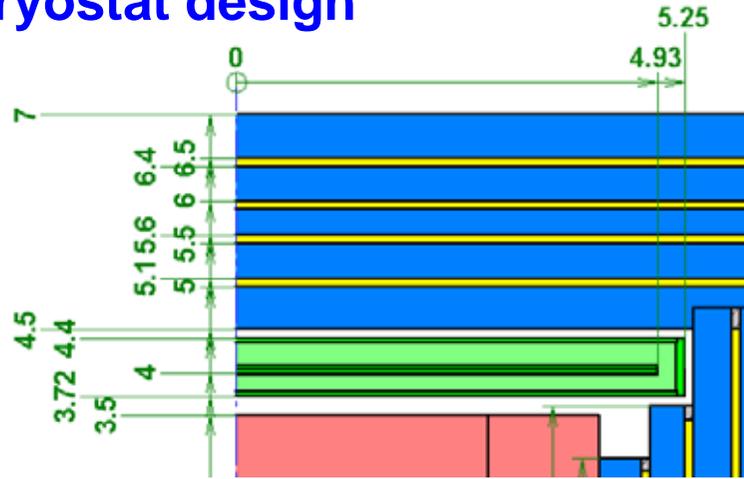


Development of High-strength Al

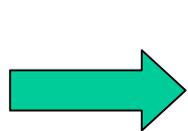


Cryostat design

Oct. 29, '04
KEK H. Yamaoka



Load condition
 Weight of the calorimeter: **2000tons**
 Weight of the solenoid : ~ **140tons**
 Vacuum : **0.1MPa**



Thickness of
 • Inner vacuum vessel
 • End plates
 were optimized.

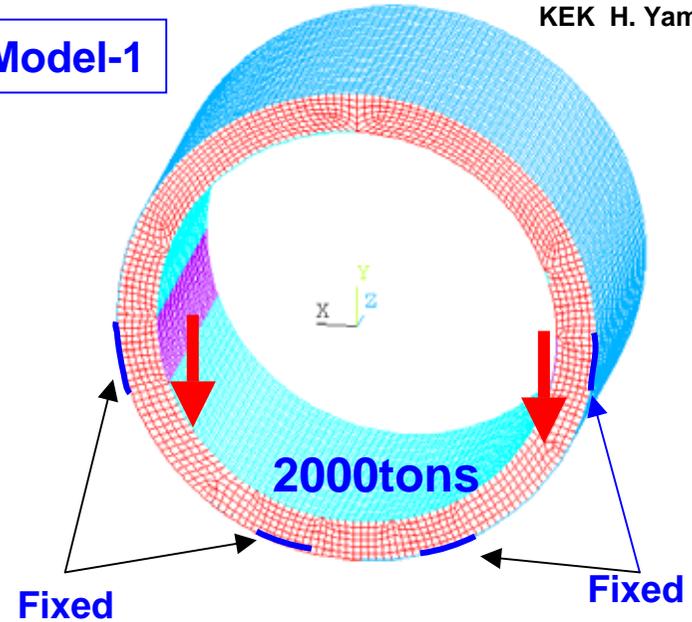
SUS304
 $\sigma_t = 530\text{MPa}$
 $\sigma_y = 210\text{MPa}$
 $\sigma_{\text{allow}} = 140\text{MPa}$

- Outer vac. vessel
 40mm thick

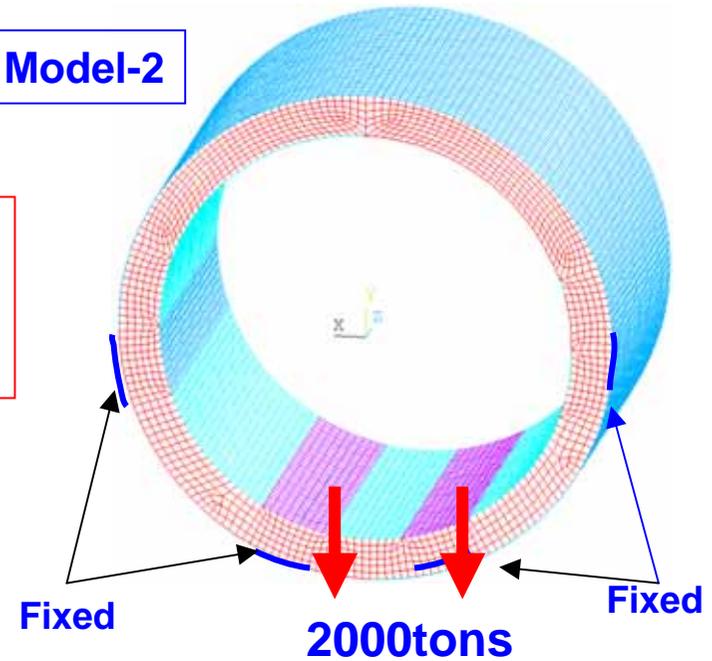
$$p = \frac{0.855}{(1-\mu^2)} \cdot \frac{0.75E}{\left(\frac{r}{t}\right)^5 \cdot \left(\frac{L}{r}\right)}$$

p : Buckling pressure
 0.1MPa x 2(safety factor)

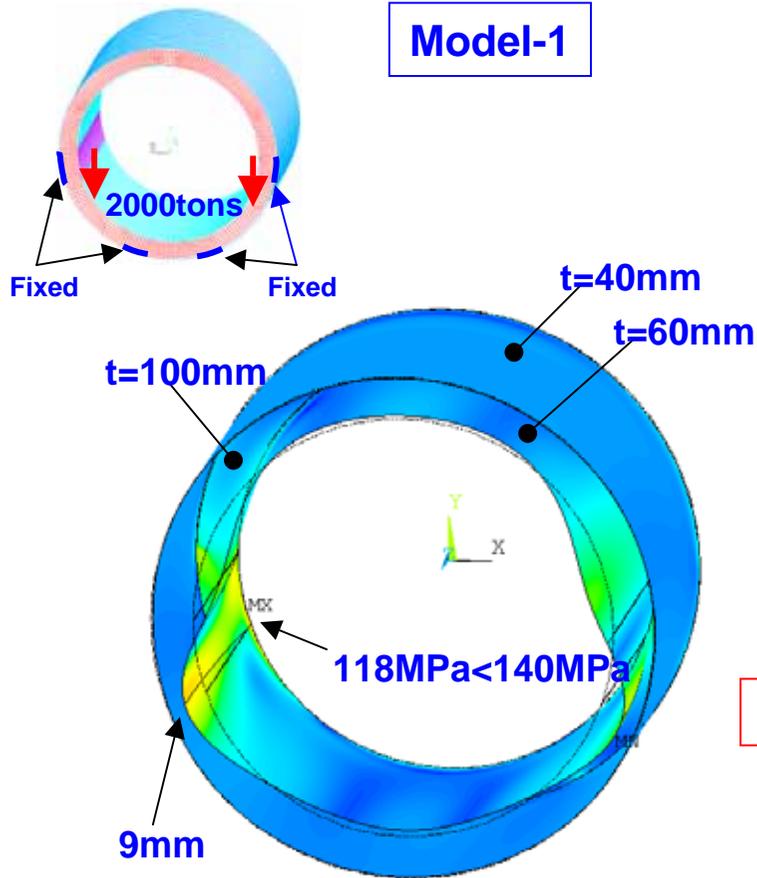
Model-1



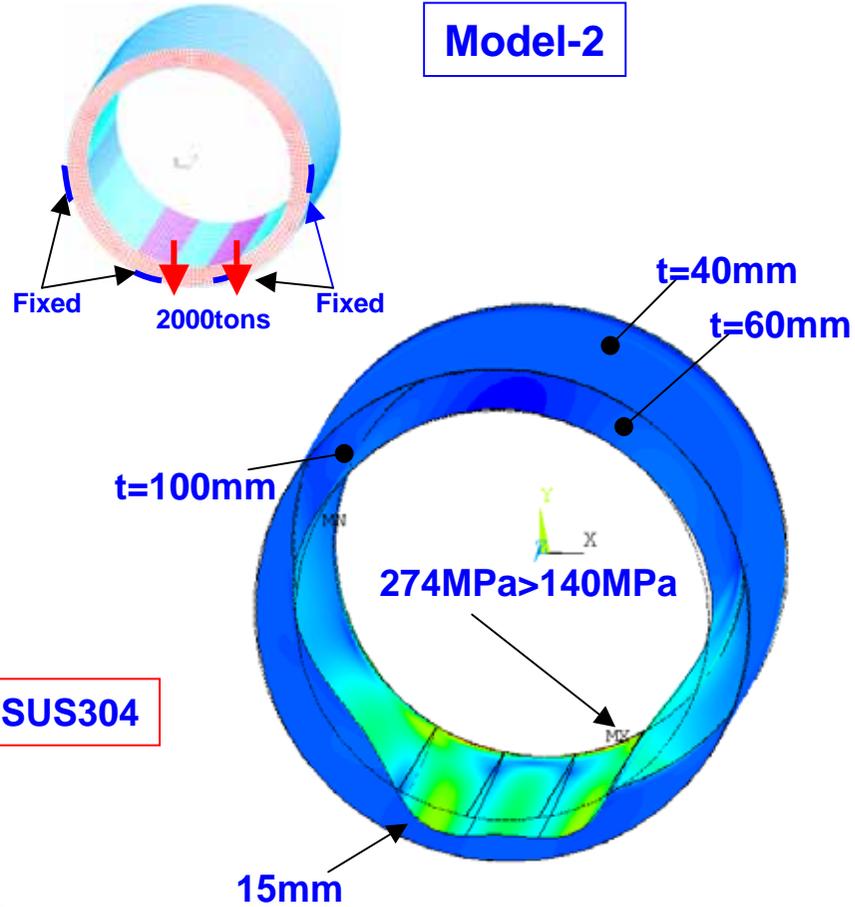
Model-2



Model-1



Model-2



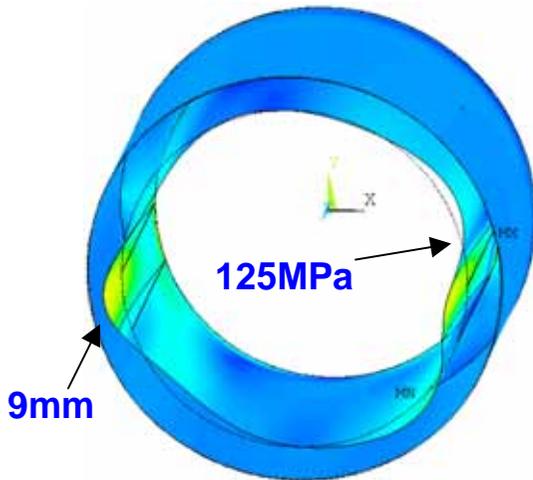
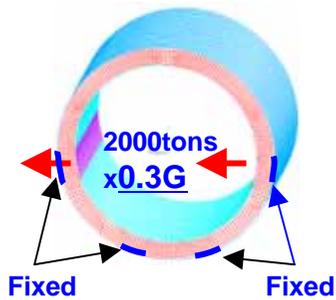
Material: SUS304

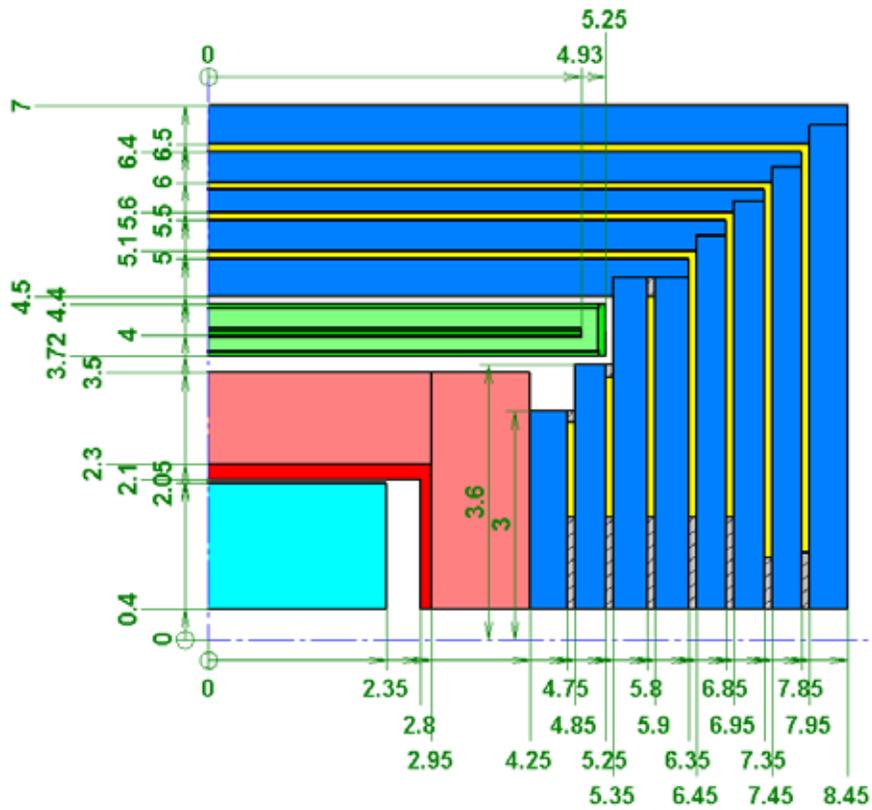
Stiffness: D

$$D = E \cdot I$$

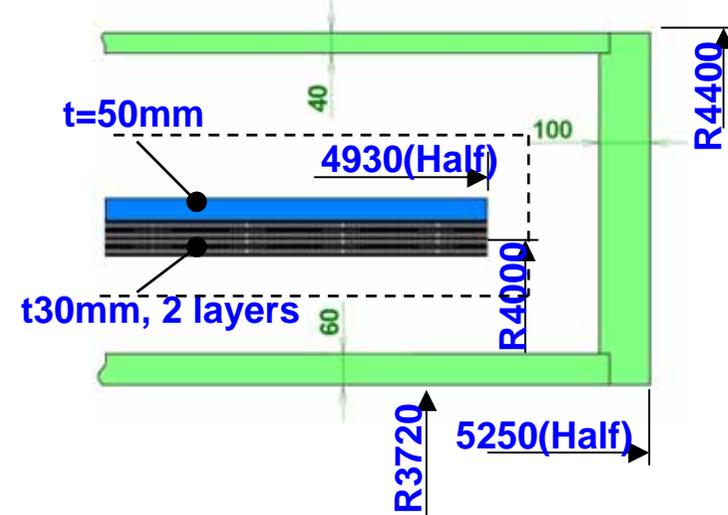
$$I = \frac{\text{Width} \cdot \text{Height}^3}{12}$$

E: Young's modulus
I: Moment of Inertia



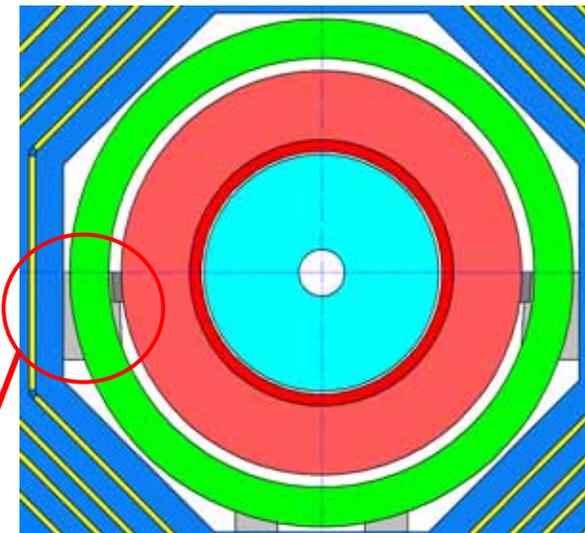


*Coil support system is not designed yet.

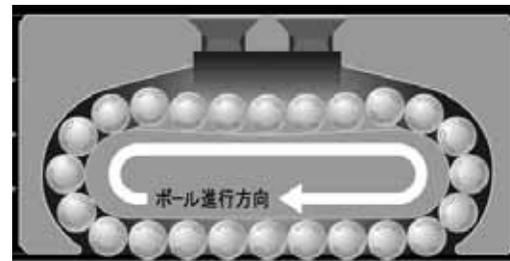
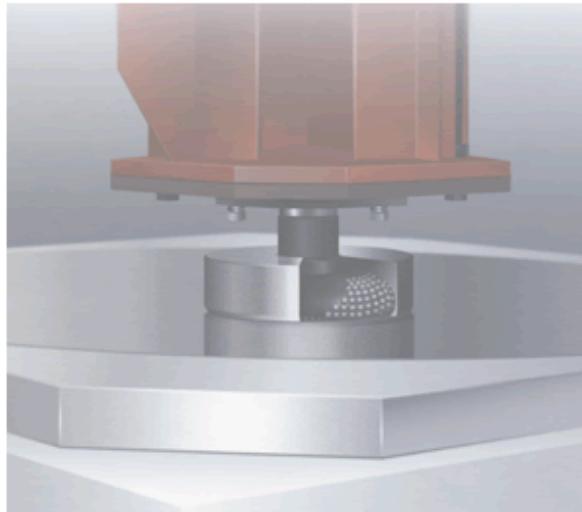
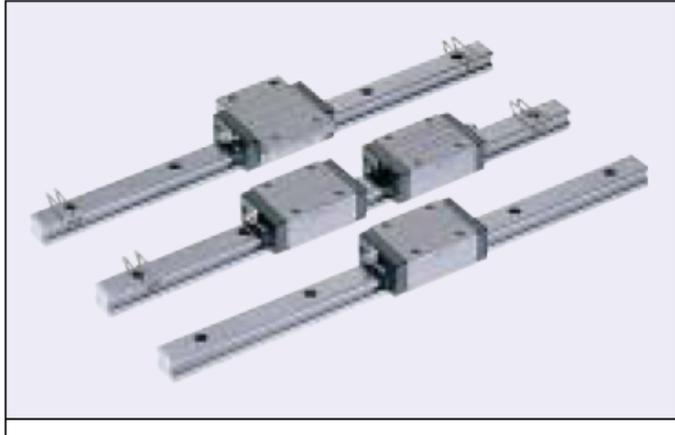


Requests to calorimeter structure;

- Calorimeter is divided to several pieces in the axial direction.
- One piece of calorimeter is stiff enough.



*Detail design is not yet done.



Feb. 14, '02 H. Y

Cost estimation of Return Yoke

Law material

¥180/kg x 11000e3kg = ¥19.8 oku

+α(10%)

19.8x1.1=21.8 oku

Machining

Total area for machining of Barrel yoke

340m²

End Yoke:

501m²

Machining cost per 1m²

¥200000/m²

Total:

(340+501)m²x20万=16.8 oku

+α(10%)、

16.8x1.1=18.5 oku

Design cost

1 oku

Cost for QC

0.5 oku

利益率

20%とすると、

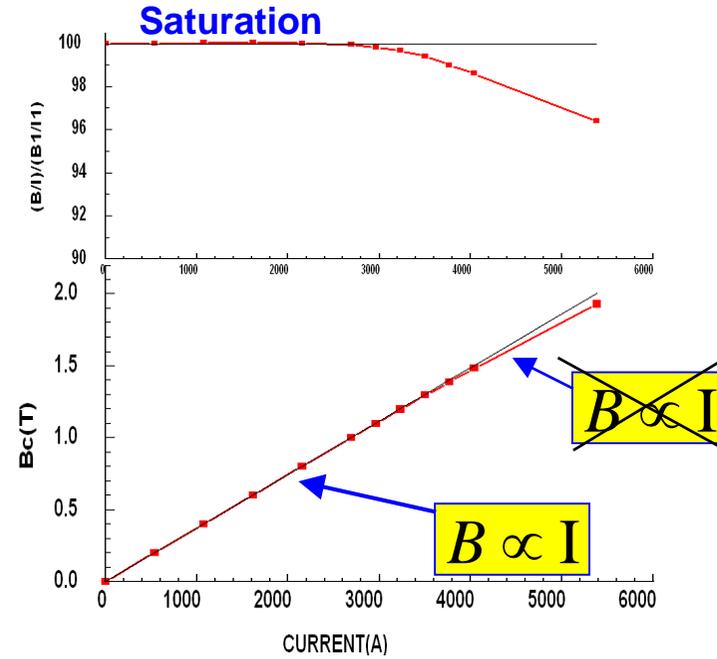
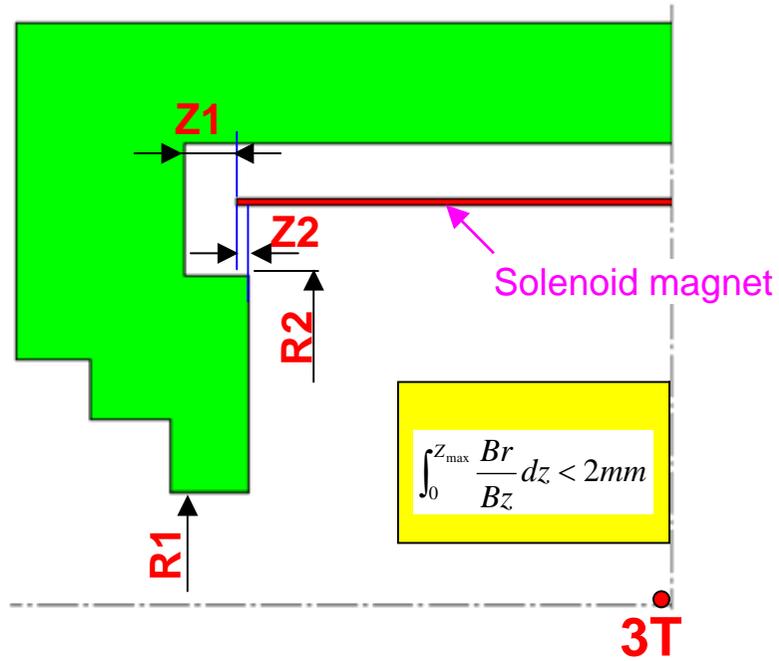
41.8x0.2=8.4 oku

Total

50.2 okux1.05=52.7 oku

Cost estimation of Solenoid

The way for improving field uniformity



- Plenty of amount of iron
- Minimize $Z1, R1$
- Optimize $Z2, R2$